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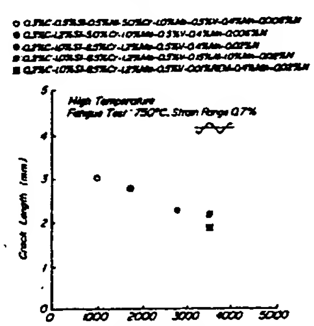
## (54) Steels for hot working press tools.

(57) A steel suitable for hot working press tool used for slab width sizing press comprises particular amounts of C, Si, Cr, Mn, Mo, V and N having a specific Cr equivalent, or particular amounts of C, Si, Mn, Mo, V, Cr and Ni having a specified Cr/Ni ratio.

*FIG. 1*

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## STEELS FOR HOT WORKING PRESS TOOLS

This invention relates to steels for hot working press tools used in the continuous reduction of slab width.

When slabs of various sizes are produced by the continuous casting method, it is necessary to provide a mold for continuous casting in correspondence to each size of the slabs, so that there is a problem of decreasing the productivity through the exchange of the mold. Therefore, it is desired to arrange various sizes of the molds into some typical sizes.

For this purpose, there has been developed a slab width sizing press (hereinafter referred to as sizing press) in which the width of the hot slab after the continuous casting is reduced in the widthwise direction over a full length of the slab ranging from the head to the tail in accordance with a size of the slab to be reduced by repeatedly applying a pressure in widthwise direction to the hot slab through a pressing tool (hereinafter referred to as anvil) every the relative feeding of the slab to the anvil. In this case, the anvil used in the sizing press is subjected to thermal load, so that the cracking due to thermal stress is apt to be caused. Therefore, the anvil having a high resistance to thermal fatigue is demanded for preventing the decrease of productivity through the exchange of the anvil.

The steels for hot working used in press die, forging die and the like have a standard according to JIS G4404 together with steels for cutting tool, impact tool, cold working die and the like, some of which are disclosed in Japanese Patent Application Publication No. 54-38,570.

These steels for hot working are sufficiently durable to ordinary hot working, but are still insufficient for use in the anvil in the sizing press. Because the anvil for the sizing press is large in the size and is continuously used for the hot slab above 1,200°C, so that the temperature of the anvil becomes high up to the deeply inside thereof as compared with the hot rolling roll and consequently excessive thermal stress is caused in the cooling and there is a problem of causing the cracking due to thermal fatigue.

It is, therefore, an object of the invention to provide steels having a high resistance to thermal fatigue and suitable for use in hot working press tools under severe use conditions as in the sizing press or the like.

According to a first aspect of the invention, the steel is a martensitic steel for hot working press tool consisting essentially of Cr-Mo-V as a basic component and containing Si, Mn and N, which is usable for the sizing press. In this case, the presence of Cr and Si improves the oxidation resistance of steels, and the presence of Si, Mo and V raises the transformation temperature and restrict the upper limit of Cr equivalent to prevent the appearance of δ-ferrite inherent to high-Cr steel, whereby the resistance to thermal fatigue is improved to prevent the cracking of the hot working press tool such as anvil or the like due to the thermal fatigue.

According to a second aspect of the invention, at least one of Al and REM (rare earth metal) is added to the steel of the first invention, whereby the oxidation resistance is improved to further enhance the resistance to thermal fatigue.

According to a third aspect of the invention, the steel is a martensitic steel for hot working press tool consisting essentially of Cr-Ni-Mo-V as a basic component and containing Si and Mn, which is usable for the sizing press. In this case, the notch-like high temperature oxide scale produced in case of low Cr and high Ni is prevented by taking Cr/Ni≥5, whereby the resistance to thermal fatigue is improved to prevent the cracking of the hot working die due to thermal fatigue.

That is, the first invention provides a steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.05-0.35 wt% (hereinafter merely shown by %), Si: 0.80-2.5%, Mn: 0.10-2.0%, Cr: 7.0-13.0%, Mo: 0.50-3.0%, V: 0.10-0.60%, N: 0.005-0.10% and the balance being iron and inevitable impurities, and satisfying Cr equivalent of not more than 16 represented by the following equation:

Cr equivalent = Cr + 6Si + 4Mo + 11V - 40C - 2Mn - 30N(wt%).

The second invention provides a steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.05-0.35%, Si: 0.80-2.5%, Mn: 0.10-2.0%, Cr: 7.0-13.0%, Mo: 0.50-3.0%, V: 0.10-0.60%, N: 0.005-0.10% and the balance being iron and inevitable impurities, and further containing at least one of Al: 0.005-0.5% and REM: 0.005-0.02%, and satisfying Cr equivalent of not more than 16 represented by the following equation:

Cr equivalent =

Cr + 6Si + 4Mo + 11V + 12Al - 40C - 2Mn - 30N(wt%).

The third invention provides a steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.10-0.45%, Si: 0.10-2.0%, Mn: 0.10-2.0%, Mo: 0.50-3.0%, V: 0.50-0.80%,



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Cr: 3.0-8.0% and Ni: 0.05-1.2%, provided that Cr/Ni≥5, and the balance being iron and inevitable impurities.

The invention will be described with reference to the accompanying drawings, wherein:

Fig. 1 is a graph showing a relation between number of cycles and crack length in the high temperature fatigue test;

Fig. 2 is a graph showing a relation between Cr equivalent and δ-ferrite content;

Fig. 3 is a graph showing a relation between Cr content and weight reduction through oxidation;

Fig. 4 is a diagrammatical view showing a notch-like scale; and

Fig. 5 is a graph showing a relation between Cr/Ni and length of notch-like scale.

The anvil aimed at the invention is subjected to not only a simple thermal stress but also a mechanical stress in a contact surface with the slab at a high temperature. As a result, the cracking is partially caused in the oxide layer, which is a starting point for the cracking through selective oxidation and thermal fatigue, resulting in the degradation of the resistance to thermal fatigue.

In order to solve this problem, steels having various chemical compositions were subjected to a high temperature fatigue test in an oxidizing atmosphere (in air) at a test temperature of 750°C and a strain range of 0.7%, during which the occurrence and growth of crack were measured. The results are shown in Fig. 1.

As seen from Fig. 1, increasing of Cr and Si contents as well as adding of Al and REM in the steel is effective to prevent the growth of cracks.

In the anvil aimed at the invention, the thermal fatigue comes into problem, so that the presence of δ-ferrite being a stress concentration source is harmful. It is necessary to prevent the appearance of δ-ferrite.

In the first and second invention, the reason why the chemical composition of the steel is limited to the above defined range is as follows:

C: 0.05-0.35%

C is required to improve the hardenability and maintain the hardness after the quenching and tempering and the strength at high temperature. Further, C forms carbides by reacting with Cr, Mo and V to thereby enhance the wear resistance and the softening resistance after the tempering. Moreover, C is necessary as an austenite forming element for preventing the appearance of δ-ferrite. If the C content is too large, the toughness is decreased and the transformation temperature is lowered, so that the upper limit should be 0.35%. On the other hand, when the C content is too small, the wear resistance is poor and the appearance of δ-ferrite is caused, so that the lower limit should be 0.05%..

Si: 0.80-2.0%

Si is added for maintaining the oxidation resistance and raising the transformation temperature. When the Si content is too large, the toughness is decreased, so that the upper limit is 2.0%. On the other hand, when it is too small, the effect is lost, so that the lower limit is 0.80%.

Mn: 0.10-2.0%

Mn is required to improve the hardenability and prevent the formation of δ-ferrite. When the Mn content is too large, the transformation temperature is lowered, so that the upper limit should be 2.0%, while when it is too small, the effect is lost, so that the lower limit should be 0.10%.

Cr: 7.0-13.0%

A part of Cr forms carbonitrides which precipitate in the matrix, whereby the wear resistance is improved. Further, the remaining Cr is soluted to improve the hardenability, whereby the hardness after the quenching and tempering and the high-temperature str ngth ar improved. Moreover, Cr is an element effective for improving the oxidation resistance at high temperature and raising the transformation temperature. When the Cr content is less than 7.0%, the effect is poor, while when it exceeds 13.0%, δ-ferrite app ars to lower th resistance to thermal fatigue, so that the Cr content is limited to a range of 7.0-13.0%.



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Mo: 0.50-3.0%

Mo is soluted into the matrix to improve the hardenability and also forms hard carbides by bonding with C to precipitate in the matrix, whereby the wear resistance is enhanced. Further, Mo enhances the softening resistance through tempering and increases the high-temperature strength, and raises the transformation temperature. When the Mo content is more than 3.0%, the toughness is decreased, while when it is less than 0.5%, the sufficient effect is not obtained, so that the Mo content is limited to a range of 0.5-3.0%.

V: 0.10-0.60%

V precipitates fine carbonitrides to enhance the softening resistance through tempering and the high-temperature strength and raise the transformation temperature. However, when the V content is too large, a coarse carbide is formed to lower the toughness, while when it is too small, the effect is not obtained, so that it is limited to a range of 0.10-0.60%.

N: 0.005-0.10%

N is added in an amount of not less than 0.005% for the improvement of high-temperature strength and the prevention of δ-ferrite formation. However, when it exceeds 0.10%, the toughness is considerably decreased, so that the upper limit is 0.10%.

In the second invention, at least one of Al: 0.005-0.2% and REM: 0.005-0.02% is included in the steel.

Al is an element for improving the toughness through an effect of fining crystal grains and further enhancing the oxidation resistance. For this purpose, Al is required to be added in an amount of 0.005%. However, when it exceeds 0.20%, coarse AlN is apt to be formed to decrease the toughness, so that the upper limit is 0.20%.

REM (rare earth element) consisting essentially of La and Ce is a component for improving the oxidation resistance. For this purpose, it is required to be included in an amount of not less than 0.005%. When the amount exceeds 0.02%, the toughness is decreased, so that the upper limit is 0.02%.

In the first and second inventions, Cr equivalent represented by the following equation is necessary to be not more than 16.

Cr equivalent = Cr + 6Si + 4Mo + 11V + 12Al-40C-2Mn-30N (wt%)

The Cr equivalent has a good relation to the appearance of δ-ferrite. In Fig. 2 are shown results for the effect of Cr equivalent on δ-ferrite content when the Cr equivalent is changed by varying the chemical composition of the steel. As seen from Fig. 2, when the Cr equivalent exceeds 16, δ-ferrite is formed, while the appearance of δ-ferrite can be prevented by restricting the Cr equivalent to not more than 16.

In the third invention, the reason why the chemical composition of the steel is limited to the above defined range is as follows:

C: 0.10-0.45%

C is required to improve the hardenability and maintain the hardness after the quenching and tempering and the strength at high temperature. Further, C forms carbides by reacting with Cr, Mo and V to thereby enhance the wear resistance and the softening resistance after the tempering. If the content of C is too large, the toughness is decreased, so that the upper limit should be 0.45%. On the other hand, when it is less than 0.10%, the above effects are not obtained, so that the lower limit should be 0.10%.

Si: 0.10-2.0%

Si is added for maintaining the oxidation resistance and raising the transformation temperature. When the Si content is too large, the toughness is decreased, so that the upper limit is 2.0%. On the other hand, when it is too small, the effect is lost, so that the lower limit is 0.10%.

Mn: 0.10-2.0%



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Mn is required to improve the hardenability. When the Mn content is too large, the $A_1$ transformation temperature is lowered, so that the upper limit should be 2.0%, while when it is too small, the effect is lost, so that the lower limit should be 0.10%.

Mo: 0.50-3.0%

Mo is soluted into the matrix to improve the hardenability and also forms hard carbides by bonding with C to precipitate in the matrix, whereby the wear resistance is enhanced. Further, Mo enhances the softening resistance through tempering and the high temperature strength, and raises the $A_1$ transformation temperature. When the Mo content is more than 3.0%, the toughness is decreased, while when it is less than 0.5%, the sufficient hardening depth is not obtained, so that the content is limited to a range of 0.5-3.0%.

V: 0.50-0.80%

V forms fine carbonitrides to enhance the softening resistance through tempering and the high-temperature strength. V makes the grain fine, whereby the toughness is increased, and raises the $A_1$ transformation temperature. However, when the V content is too large, a coarse carbide is formed to decrease the toughness, while when it is too small, the effect is not obtained, so that it is limited to a range of 0.5-0.8%.

Cr: 3.0-8.0%

A part of Cr forms carbides to precipitate in the matrix to thereby improve the wear resistance, while the remaining Cr is soluted to increase the hardenability. Moreover, the hot working die for reducing the slab width comes into contact with the high temperature slabes which raise the temperature of the surface of the die itself, so that it is required to have an oxidation resistance at high temperature. In this connection, the presence of Cr can improve the latter property. However, as seen from Fig. 3 showing an influence of Cr content upon the weight loss through oxidation at high temperature, when the content is less than 3.0%, the effect is insufficient, while when it exceeds 8.0%, the effect is saturated and becomes disadvantageous in economy, so that the Cr content is limited to a range of 3.0-8.0%. Moreover, Fig. 3 shows the experimental results when heating in air at 100° C for 48 hours.

Ni: 0.05-1.2%

Ni is an element useful for the improvement of toughness and hardenability and is added in an amount of not less than 0.05%. However, when the content exceeds 1.2%, the addition becomes disadvantageous in economy, so that the Ni content is limited to a range of 0.05-1.2%.

On the other hand, when the steel is used in a large die for the sizing press, it is exposed to high temperature in use and subjected to large thermal stress in the cooling, so that the cracking due to thermal fatigue is a greatest problem. In this connection, the presence of Ni decreases the resistance to thermal fatigue in the oxidizing atmosphere. That is, the presence of Ni promotes the selective oxidation and forms a notch-like scale through oxidation at high temperature as shown in Fig. 4. The notch-like scale further enlarges the cracking and decreases the resistance to thermal fatigue.

Fig. 5 shows an influence of Cr/Ni upon depth of notch-like scale, from which it is apparent that the formation of notch-like scale is restrained by the addition of Cr together with Ni addition. The notch-like scale as shown in Fig. 4 is measured on test samples when steel ingots containing C: 0.40%, Si: 1.0%, Mn: 0.4%, Mo: 1.25% and V: 0.5% and further variable amount of Ni: 0.05-1.65% and Cr: 1.21-7.9% were heated at 900° C for 15 hours and cooled in air, and the results are shown in Fig. 5 in comparison with the ratio Cr/Ni.

As seen from Fig. 5, when Cr/Ni≧5, the length of notch-like scale can be restrained to not more than 10 µm. That is, the formation of notch-like scale can substantially be suppressed and the resistance to thermal fatigue can be well held.

The steels according to the invention can be produced by melting a particular steel in a converter or an electric furnace, producing a steel ingot or slab from the melt through an ingot making or continuous casting



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method, forging or rolling it, subjecting to a heat treatment inclusive of normalizing-annealing-quenching-tempering. Then, the resulting steel is shaped into a given form through machining and is applied to the sizing press. Moreover, the normalizing-annealing may be omitted in accordance with the steel composition and the steel form.

The following examples are given in illustration of the invention and are not intended as limitations thereof.

## Example 1

A steel having a chemical composition as shown in the following Table 1 was melted in a converter, which was made into an ingot. Then, the ingot was forged into a bloom having a square of 450 mm, which was normalized at 1,000°C for 10 hours and annealed at 750°C for 15 hours. Thereafter, the bloom was subjected to rough machining and further to a heat treatment including oil quenching at 1,040°C for 10 hours and tempering at 630°C for 12 hours, which was finished into an anvil of given size and applied to a test in the sizing press. The crack depth measured in the test is also shown in Table 1.

Table 1

| Run No. | Chemical composition (wt%) | | | | | | | | | | * Cr equivalent | ** Crack depth (mm) | Remarks |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | C | Si | Mn | Cr | Mo | V | N | Al | REM | others | | | |
| 1 | 0.41 | 0.38 | 0.77 | 2.45 | 1.29 | 0.51 | 0.004 | 0.003 | - | Ni:1.33 | -7.84 | more than 60 | Comparative |
| 2 | 0.40 | 0.25 | 0.73 | 1.10 | 0.23 | - | 0.003 | 0.005 | - | - | -13.97 | more than 60 | Example |
| 3 | 0.05 | 0.35 | 0.21 | 12.45 | 0.40 | 0.10 | 0.020 | 0.002 | - | Ni:4.05 | -1.95 | more than 60 | |
| 4 | 0.05 | 0.65 | 0.35 | 13.15 | 0.40 | 0.08 | 0.008 | 0.005 | - | - | 16.65 | 31 | |
| 5 | 0.30 | 0.55 | 0.41 | 6.20 | 1.26 | 0.58 | 0.006 | 0.003 | - | - | 7.96 | 22 | |
| 6 | 0.20 | 1.01 | 0.39 | 8.10 | 1.25 | 0.48 | 0.010 | 0.003 | - | - | 15.40 | 4 | First |
| 7 | 0.12 | 0.95 | 1.20 | 9.53 | 1.05 | 0.31 | 0.024 | 0.003 | - | - | 14.96 | 3 | invention |
| 8 | 0.25 | 0.99 | 0.42 | 8.30 | 1.15 | 0.50 | 0.012 | 0.018 | | - | 13.36 | 3 | Second |
| 9 | 0.24 | 1.22 | 1.40 | 12.50 | 1.20 | 0.25 | 0.051 | 0.008 | 0.008 | - | 13.54 | 2 | invention |
| 10 | 0.13 | 1.02 | 0.90 | 9.62 | 1.02 | 0.28 | 0.020 | 0.002 | 0.010 | - | 15.32 | 2 | |
| 11 | 0.26 | 1.03 | 1.00 | 9.11 | 1.31 | 0.32 | 0.008 | 0.24 | - | - | 14.29 | 3 | |

* Cr equivalent = Cr + 6Si + 4Mo + 11V + 12Al - 40C - 2Mn - 30N(-4Ni)

** Crack depth after the forging of 3000 slabs in sizing press

## Example 2

A steel having a chemical composition as shown in the following Table 2 was melted in a converter, which was made into an ingot. Then, the ingot was forged into a bloom having a square of 450 mm, which was subjected to a heat treatment including quenching and tempering and then finished into an anvil of given size for hot working press tool and applied to a test in the sizing press. The length of notch-like scale after the heat treatment at 950°C for 15 hours and the crack depth measured in the test are also shown in Table 2.



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Table 2

| Run No. | C | Si | Mn | P | S | Ni | Cr | Mo | V | Cr/Ni | * Length of notch-like scale (μm) | ** Crack depth (mm) | Remarks |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 0.55 | 0.20 | 0.80 | 0.002 | 0.004 | 1.65 | 1.21 | 0.36 | 0.16 | 0.73 | 96 | - | Comparative Example |
| 2 | 0.41 | 0.38 | 0.77 | 0.019 | 0.006 | 1.33 | 2.45 | 1.29 | 0.51 | 1.84 | 45 | more than 60 | |
| 3 | 0.35 | 0.99 | 0.39 | 0.003 | 0.004 | 1.50 | 4.75 | 1.30 | 0.54 | 3.16 | 15 | 21 | |
| 4 | 0.40 | 0.50 | 0.40 | 0.015 | 0.005 | 0.50 | 5.00 | 1.25 | 0.51 | 10.0 | 7 | 5 | Third invention |
| 5 | 0.35 | 1.30 | 0.39 | 0.003 | 0.004 | 0.05 | 4.82 | 1.27 | 0.52 | 96.4 | 5 | - | |
| 6 | 0.35 | 1.95 | 0.38 | 0.003 | 0.003 | 0.03 | 4.72 | 1.26 | 0.52 | 94.4 | 3 | - | |
| 7 | 0.36 | 1.31 | 0.39 | 0.004 | 0.005 | 0.07 | 7.90 | 1.35 | 0.56 | 112.9 | 5 | - | |
| 8 | 0.30 | 0.55 | 0.41 | 0.005 | 0.003 | 0.20 | 4.93 | 1.26 | 0.58 | 24.7 | 4 | 7 | |
| 9 | 0.31 | 0.60 | 0.42 | 0.005 | 0.003 | 0.15 | 5.12 | 1.30 | 0.55 | 34.1 | 5 | 6 | |
| 10 | 0.30 | 1.25 | 0.56 | 0.004 | 0.003 | 0.08 | 5.90 | 0.90 | 0.59 | 73.8 | 4 | - | |
| 11 | 0.29 | 1.45 | 0.62 | 0.004 | 0.002 | 0.06 | 6.20 | 0.85 | 0.61 | 103.3 | 5 | - | |
| 12 | 0.30 | 1.32 | 0.56 | 0.004 | 0.002 | 0.15 | 6.15 | 0.92 | 0.60 | 41.0 | 6 | 3 | |

* measured at room temperature after heating at 950°C for 15 hours in air

** Crack depth (mm) after forging of 1000 slabs in sizing press (-: not measured)



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As mentioned above, according to the invention, the improvement of the resistance to thermal fatigue, which is lacking in the conventional steel for hot working press tool, can be achieved, so that the steels according to the invention can advantageously be applied to hot working press tool suitable for slab width sizing press.

## Claims

1. A steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.05-0.35 wt%, Si: 0.80-2.5 wt%, Mn: 0.10 2.0 wt%, Cr: 7.0-13.0 wt%, Mo: 0.50-3.0 wt%, V: 0.10-0.60 wt%, N: 0.005-0.10 wt% and the balance being iron and inevitable impurities, and satisfying Cr equivalent of not more than 16 represented by the following equation:
Cr equivalent = Cr + 6Si + 4Mo + 11V - 40C - 2Mn - 30N(wt%).

2. A steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.05-0.35 wt%, Si: 0.80-2.5 wt%, Mn: 0.10-2.0 wt%, Cr: 7.0-13.0 wt%, Mo: 0.50-3.0 wt%, V: 0.10-0.60 wt%, N: 0.005-0.10 wt% and the balance being iron and inevitable impurities, and further containing at least one of Al: 0.005-0.5 wt% and REM: 0.005-0.02 wt%, and satisfying Cr equivalent of not more than 16 represented by the following equation:
Cr equivalent =
Cr + 6Si + 4Mo + 11V + 12Al - 40C - 2Mn - 30N(wt%).

3. A steel for hot working press tool used for continuously reducing a slab width, consisting essentially of C: 0.10-0.45 wt%, Si: 0.10-2.0 wt%, Mn: 0.10-2.0 wt%, Mo: 0.50-3.0 wt%, V: 0.50-0.80 wt%, Cr: 3.0-8.0 wt% and Ni: 0.05-1.2 wt%, provided that Cr/Ni≥5, and the balance being iron and inevitable impurities.



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FIG_ 1

○:0.3%C-0.5%Si-0.5%Ni-5.0%Cr-1.0%Mo-0.5%V-0.4%Mn-0.006%N
◐:0.3%C-1.2%Si-5.0%Cr-1.0%Mo-0.5%V-0.4%Mn-0.006%N
●:0.2%C-1.0%Si-8.5%Cr-1.2%Mo-0.5%V-0.4%Mn-0.02%N
●:0.2%C-1.0%Si-8.5%Cr-1.2%Mo-0.5%V-0.15%Al-1.0%Mn-0.02%N
✖:0.2%C-1.0%Si-8.5%Cr-1.2%Mo-0.5%V-0.01%REM-0.4%Mn-0.02%N

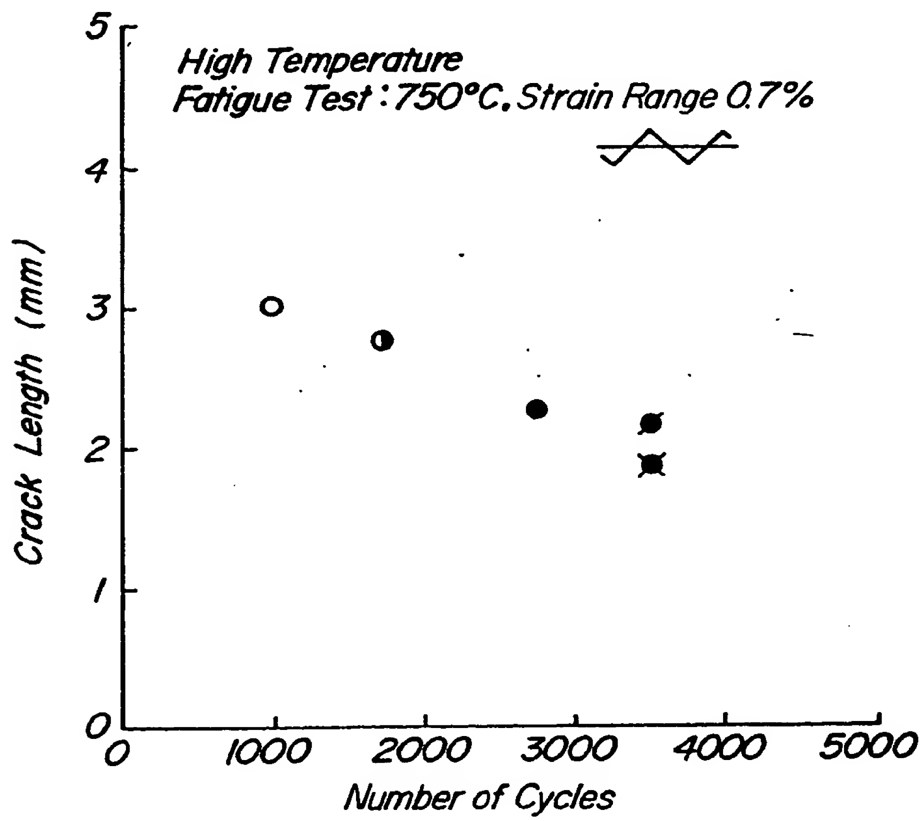


FIG_2

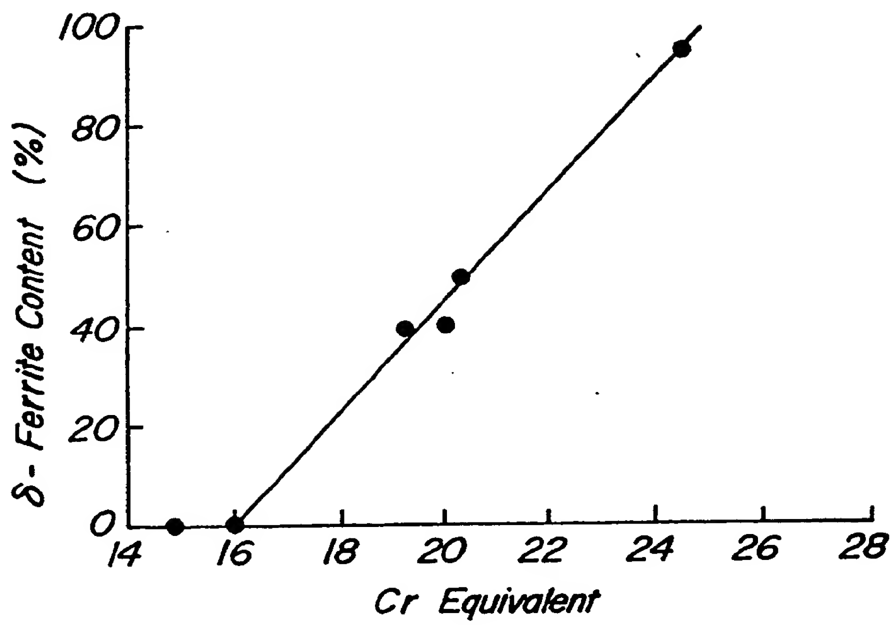

100
80
60
40
20
0
14
16
18
20
22
24
26
28
δ- Ferrite Content (%)
Cr Equivalent

FIG_3

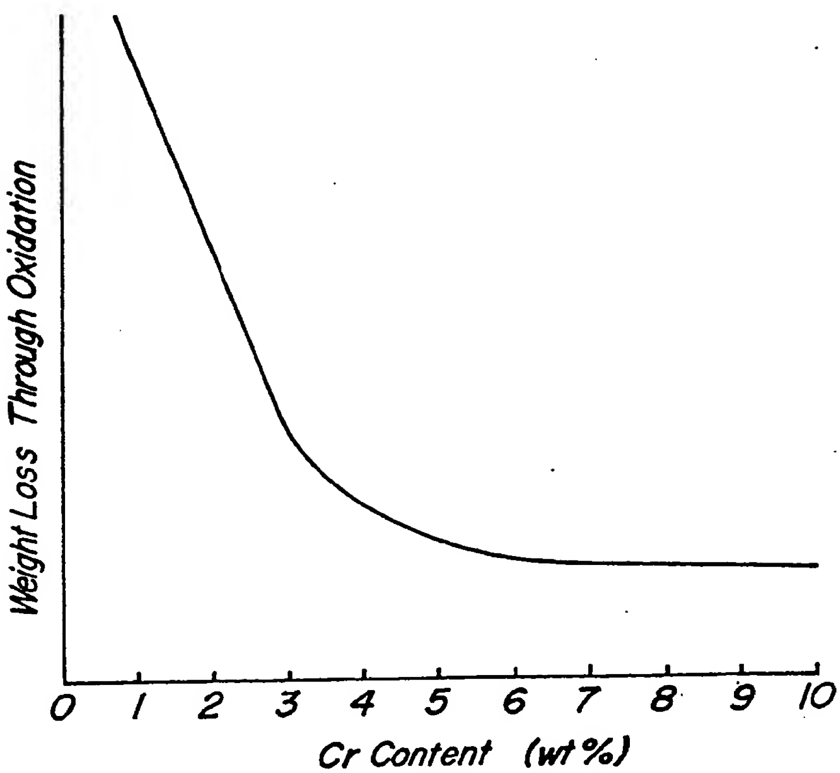
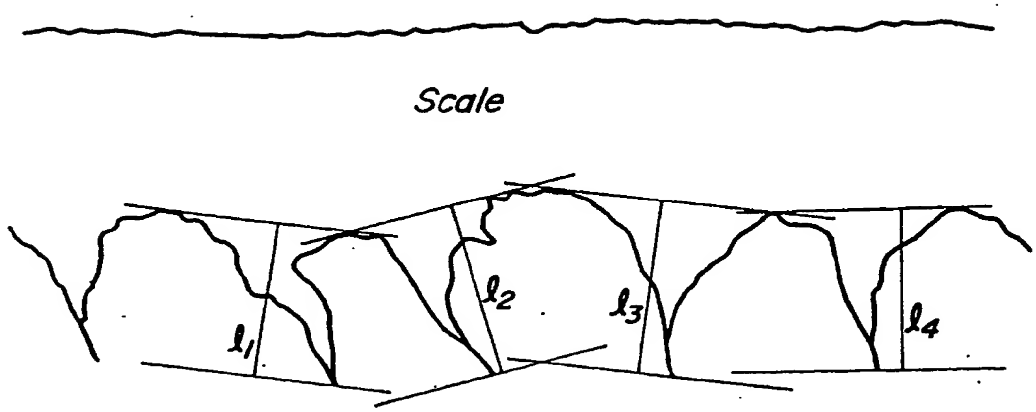
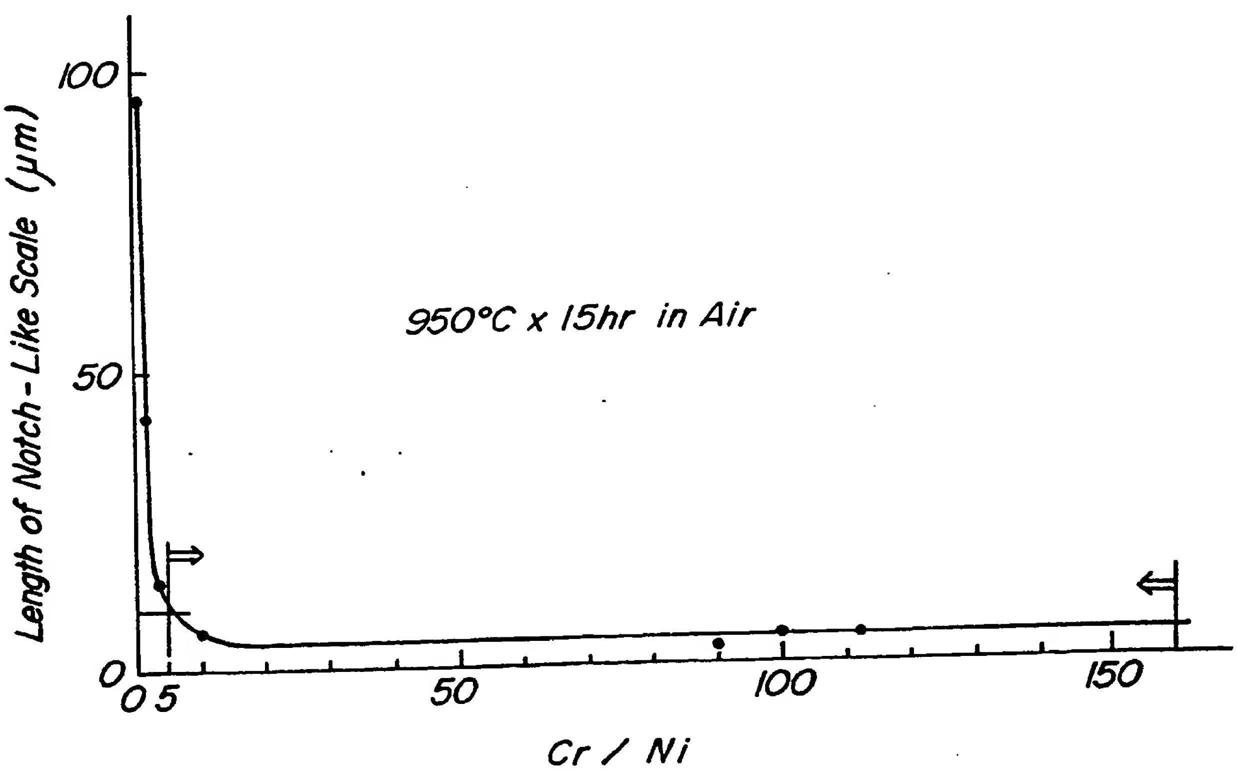


FIG_4




Depth of Notch-Like Scale $l = \frac{l_1 + l_2 + \cdots + l_{10}}{10}$

FIG_5


Length of Notch-Like Scale (μm)
100
50
0
950°C x 15hr in Air
0 5
50
100
150
Cr / Ni

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Office européen des br vets

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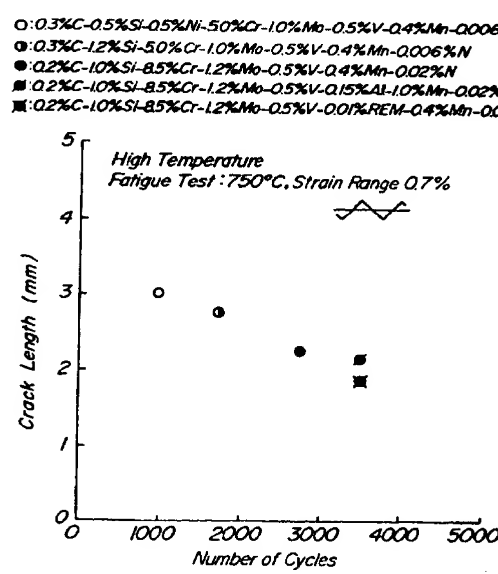
## (54) Steels for hot working press tools.

(57) A steel for hot working press tool consisting essentially of C: 0.05-0.35 wt%, Si: 0.80-2.5 wt%, Mn: 0.10-2.0 wt%, Cr: 7.0-13.0 wt%, Mo: 0.50-3.0 wt%, V: 0.10-0.60 wt%, N: 0.005-0.10 wt%, the balance being iron and inevitable impurities, and optionally containing Al: 0.005-0.5 wt% and/or REM: 0.005-0.02 wt%, with the proviso that
Cr equivalent =
Cr + 6Si + 4Mo + 11V + 12Al - 40C - 2Mn - 30N(wt%) ≤ 16.

FIG_1




EP 0 338 133 A3



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European
Patent Office

# EUROPEAN SEARCH REPORT

Application Number

EP 88 12 1328

## DOCUMENTS CONSIDERED TO BE RELEVANT

| Category | Citation of document with indication, where appropriate, of relevant passages | Relevant to claim | CLASSIFICATION OF THE APPLICATION (Int. Cl.5) |
|---|---|---|---|
| X | EP-A-0 219 089 (SUMITOMO METAL INDUSTRIES)<br>* claims 1,2,5,6 * *<br>– – – | 1-3 | C 22 C 38/22<br>C 22 C 38/24<br>C 22 C 38/34 |
| X | DE-A-2 042 394 (NIPPON KOKAN K.K.)<br>* claims 1,3 * & GB-A-1 290 412 *<br>– – – | 1 | |
| A | US-A-2 693 413 (KIRKBY ET AL.)<br>* complete document* & GB-A-687 899 *<br>– – – | 1-3 | |
| A | EP-A-0 207 052 (VEREINIGTE EDELSTAHLWERKE AKTIENGESELLSCHAFT (VEW))<br>* claim 2 ; column 3 and 4, table on the upper half of the page* *<br>– – – – – | 1-3 | |
| | | | TECHNICAL FIELDS SEARCHED (Int. Cl.5) |
| | | | C 22 C |

The present search report has been drawn up for all claims

| Place of search | Date of completion of search | Examiner |
|---|---|---|
| The Hague | 23 December 91 | LIPPENS M.H. |

CATEGORY OF CITED DOCUMENTS

X: particularly relevant if taken alone
Y: particularly relevant if combined with another document of the same catagory
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